# Power Options & Alternatives

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# Wind Turbine Performance Modeling

It works! Modeled results are within **1.2%** of the output of the output of a turbine at the South Pole.

Raytheon Wind Turbine: ARE110-HV (2.5kW turbine) on a twelve meter tower.

April only month with no turbine problems

Logs from UT.. April 241.5 kWh

Model Predictions 244.19 kWh

Note difference explainable as we don't know what time the UT's made their rounds.



# How Does The Model Work?

#### **RPSC Weather Data**

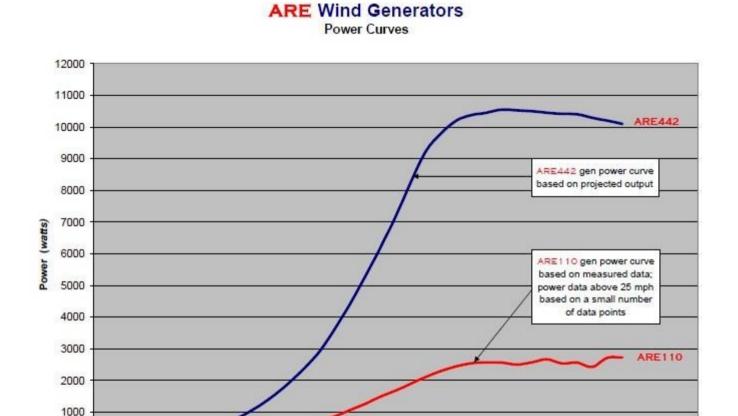
Raytheon provides weather data with one minute samples of wind speed, direction, temperature and pressure. All wind speed and direction measurements where taken at 10 meters.

# **Poor Quality**

One must correct for poor data quality. Over the course of April of this year they are actually missing 3 days worth of samples. Luckily these samples are spread very uniformly over the month so missing samples are assumed to be identical to the sample before them.

0 +

#### **Power Curves:**



Is defined for pressure at MSL with standard pressure and temperature. A curve was fit to this power curve.

15

20

Wind Speed (mph)

25

30

40

35

10

# Derating for altitude:

Wind turbines: fundamentals, technologies, application, economics Page 509, section 14.4.2 - Air Density

```
p = absolute pressure - > kPa
R = specific gas constant for dry air ( 287.05 J/(kg*K))
T = absolute temp ( deg K )
NIST standard temperature and pressure:
20 deg C, 101.325 kPa
Rho = 101325. / ( 287.05 * (20+273.15)) = 1.2041183
```

wattsAtAltitude = wattsAtSeaLevel \* ( densityAtAltitude / densityAtSealevel)

#### **Modeling For Tower Height:**

Raytheon's wind turbine is on a twelve meter tower. The Meteorological Office only measures wind speed and direction at ten meters off the surface.

Aerodynamic roughness as a function of wind direction over asymmetric surface elements Boundary-layer Meteorology, B.S. Jackson, J.J. Carroll 1978

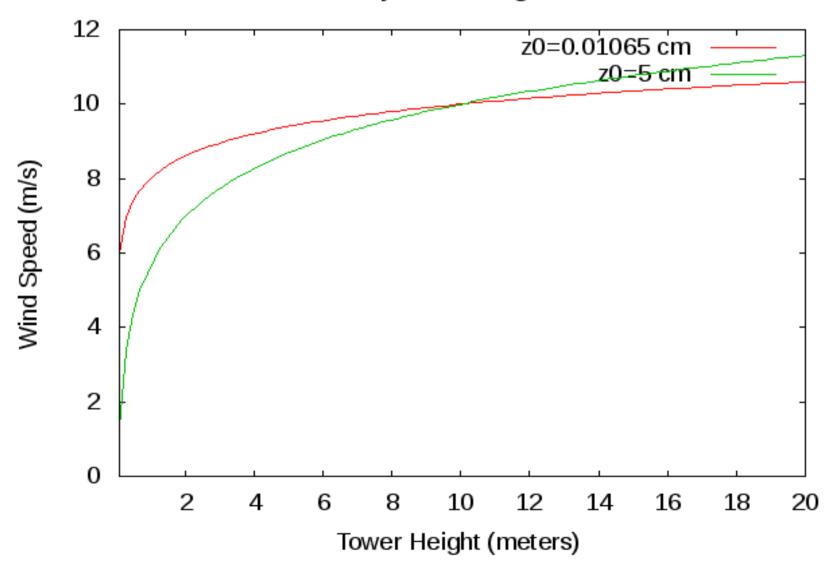
Available at: http://www.idl.ku.edu/ara/AARPS/Documents/Structural/Jackson&Carroll.pdf

The above reference measured the aerodynamic roughness as a function of wind direction at the South Pole during the winter of 1975. Wind direction matters because of sastrugi structure!

# **Does Wind Direction Really Matter?**

The extremes: z0=0.1065cm (10-15 degrees) z0=5cm (60-100 degrees) Remember, power in wind goes by the cube of the wind speed.

Jackson & Carroll Aerodynamic Roughness At The South Pole



#### **Summary of results:**

April only month with no turbine problems

Logs from UT.. April 241.5 kWh

Model Predictions 244.19 kWh

The difference is explainable as we don't know what time the UT's made their rounds.

Model source code and associated data is available at http://www.icecube.wisc.edu/~mnewcomb/hawaii

**NOTE:** Current power budget calls for a draw of 365 watts for 24 hours for 30 days = 262.8 kWh, 2.5kW turbine will not produce enough power for 100% uptime for this month.

# Applying the model to a new turbine:

Bergey XL1 (kWh per month per year) on a 20 meter tower

|      | Jan   | Feb   | Mar   | Apr   | May   | June  | July  | Aug   | Sep   | Oct   | Nov   | Dec   |
|------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 2005 | 57.8  | 195.1 | 233.2 | 299.4 | 268.8 | 284.4 | 180.5 | 317.3 | 324.9 | 283.3 | 183.5 | 201.8 |
| 2006 |       | 94.0  |       | 306.4 | 364.9 | 248.0 | 223.1 | 233.8 | 216.6 | 186.5 | 188.2 | 77.7  |
| 2007 | 131.8 | 108.4 | 186.8 | 196.3 | 316.0 | 437.1 | 299.1 | 236.4 | 218.6 | 270.6 | 110.8 |       |
| 2008 | 79.5  | 128.2 | 211.0 | 198.0 | 91.8  | 66.5  | 186.8 | 382.3 | 249.0 | 187.8 |       |       |
| 2009 | 78.2  | 259.2 |       | 211.9 |       | 325.2 | 224.6 | 233.4 | 303.3 | 271.3 | 213.9 | 71.8  |

#### Results:

**Bold** – sufficient power for 100% uptime

The model estimates at BEST that 40% of April's and 20% of July's would have enough power for 100% uptime. This is assuming a LARGE 20 meter tower!

# Another Option:

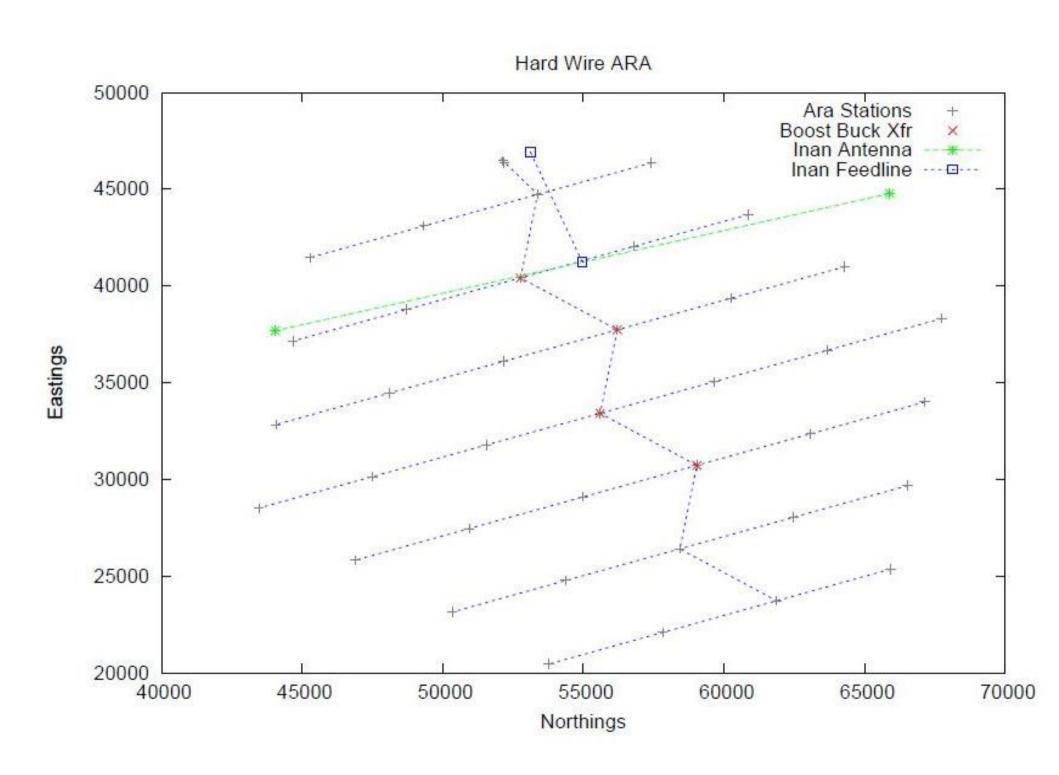
Run power cables to every station!

Mark Thoma's initial design calls for 600 VAC to be sent to each station with a step down transformer to bring the voltage down to 120VAC. Design assumes a 134 watt draw at each station. All cabling to be unshielded direct burial cable. The main feed line will require four buck boost transformers.

Cable installation to NSF required depth (~2 feet as per op-s-346-1) done by furrow plow attached to the back of a Caterpillar tractor. Mark Thoma and Dennis Dueling estimate a 1 to 3 mph trenching speed.

Note: EMI considerations need to be taken into account. What are the requirements?

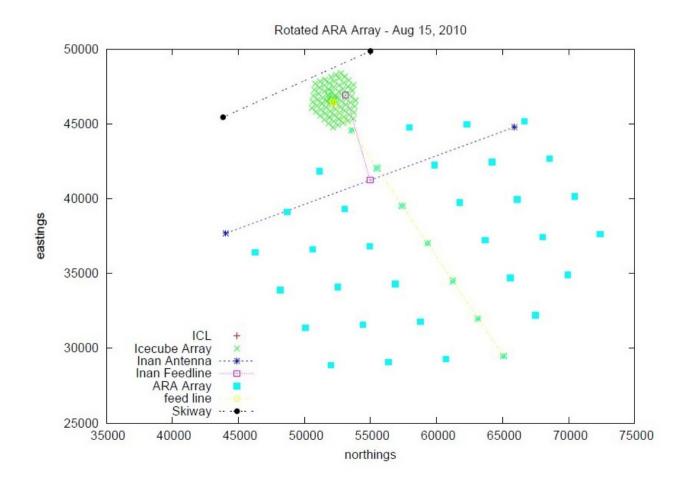
Estimated material cost: \$256K



# A Rotated ARA Array

A slight rotation and translation of the current ARA geometry cuts 3.23 KM of cable from the requirements (reducing costs to \$244K) AND moves stations farther away from the INAN antenna.

According to the 2004-2005 NSF as builts we will not have any station interference.



# **Estimated Tuned Geometry Costs:**

|   |     |        |                |           |                   | Voltage |               |              |             |           | End to end drop |        |   |             |               |           |      |          |
|---|-----|--------|----------------|-----------|-------------------|---------|---------------|--------------|-------------|-----------|-----------------|--------|---|-------------|---------------|-----------|------|----------|
|   | 1.3 | 3 Km X | Super Clusters | Watts/row | Watts progressive |         | 600 Wire size | Resistance   | L of Branch | ah .      | Voltage drop    | % drop | Number of Xfrm * cost   | Cost of xfm | n Cost of rur | n Disconn | nect |          |
| 1 |     | 3      | 3              | 402       | 402               |         | 0.67          | 14           | 5.06        | 13092.00  | 44.3            | .38    | 7.40  | 484         | 121           | 13092     | 500  |          |
|   |     | 3      | 3              | 402       | 402               |         | 0.67          | 14           | 5.06        | 13092.00  | 44.3            | .38    | 7.40  | 363         | 121           | 13092     | 500  |          |
|   | 2   | 3      | 3              | 402       | 402               |         | 0.67          | 14           | 5.06        | 13092.00  | 44.3            | .38    | 7.40  | 484         | 121           | 13092     | 500  |          |
|   |     | 3      | 3              | 402       | 402               |         | 0.67          | 14           | 5.06        | 13092.00  | 44.3            | .38    | 7.40  | 363         | 121           | 13092     | 500  |          |
|   | 3   | 3      | 3              | 402       | 402               |         | 0.67          | 14           | 5.06        | 13092.00  | 44.5            | .38    | 7.40  | 484         | 121           | 13092     | 500  |          |
|   |     | 3      | 3              | 402       | 402               |         | 0.67          | 14           | 5.06        | 13092.00  | 44.5            | .38    | 7.40  | 363         | 121           | 13092     | 500  |          |
|   | 4   | 3      | 3              | 402       | 402               |         | 0.67          | 14           | 5.06        | 13092.00  | 44.3            | .38    | 7.40  | 484         | 121           | 13092     | 500  |          |
|   |     | 3      | 3              | 402       | 402               |         | 0.67          | 14           | 5.06        | 13092.00  | 44.3            | .38    | 7.40  | 363         | 121           | 13092     | 500  |          |
|   | 5   | 2      | 2              | 268       | 268               |         | 0.45          | 14           | 5.06        | 8728.00   | 19.7            | .73    | 3.29  | 363         | 121           | 8728      | 500  |          |
|   |     | 2      | 2              | 268       | 268               |         | 0.45          | 14           | 5.06        | 8728.00   | 19.7            | .73    | 3.29  | 242         | 121           | 8728      | 500  |          |
|   | 6   | 1      | 1              | 134       | 134               |         | 0.22          | 14           | 5.06        | 4364.00   | 4.5             | .93    | 0.82  | 242         | 121           | 4364      | 500  |          |
|   |     | 1      | 1              | 134       | 134               |         | 0.22          | 14           | 5.06        | 4364.00   | 4.              | .93    | 0.82  | 121         | 121           | 4364      | 500  |          |
|   | 7   | 1      | 1              | 134       | 134               |         | 0.22          | 14           | 5.06        | 4364.00   | 4.              | .93    | 0.82  | 121         | 121           | 4364      | 500  |          |
|   |     |        |                |           |                   |         |               | Total length | į Y         | 135284.00 | i               |        | Maria de la companya della companya della companya della companya de la companya della companya | 4477        | 1             | 35284     | 6500 | 146      |
|   | 7   | 1      | 1              |           |                   |         |               | 14           | 5.06        | 4364.00   | 4.9             |        |   | 121         |               | 1         |      | 4364 500 |

| Hom | ne Run KM |               | ohms/K feet  | A.   |          |              |        |           |           |        |                |          |          |
|-----|-----------|---------------|--------------|------|----------|--------------|--------|-----------|-----------|--------|----------------|----------|----------|
|     | 7.98      | 600 Wire size | Resistance   | A.   | L to Xfr | Voltage drop | % drop | # of Xfrs | Cost of x | drm Co | ost of run Dis | sconnect |          |
| 7   | 134       | 0.22          | 14           | 5.06 | 436      | 64           | 4.93   | 0.82      |           |        | 4364           |          |          |
| 6   | 536       | 0.89          | 14           | 5.06 | 436      | 64 1         | 9.73   | 3.29      |           |        | 4364           |          |          |
| 5   | 1206      | 2.01          | 14           | 5.06 | 436      | 64 4         | 4.38   | 7.40      | 1         | 3300   | 4364           | 500      |          |
| 4   | 2144      | 3.57          | 12           | 3.18 | 436      | 64 4         | 9.59   | 8.26      | 1         | 3300   | 5629.56        | 500      |          |
| 3   | 3082      | 5.14          | 10           | 2    | 436      | 64 4         | 4.83   | 7.47      | 1         | 3300   | 7069.68        | 500      |          |
| 2   | 4020      | 6.70          | 10           | 2    | 436      | 64 5         | 8.48   | 9.75      | 1         | 3300   | 7069.68        | 500      |          |
| 1   | 4958      | 8.26          | 6            | 0.81 | 436      | 64 2         | 9.14   | 4.86      |           |        | 25223.92       |          |          |
| 0   | 4958      | 8.26          | 6            | 0.81 | 436      | 64 2         | 9.13   | 4.85      |           |        | 25223.92       |          |          |
|     |           |               | Total length | 1    | 3491     | 12           |        |           |           | 13200  | 83308.76       | 2000     | 98508.7  |
|     |           |               |              |      |          |              |        |           |           |        | To             | tal cost | 244769.7 |
|     |           |               |              |      |          |              |        |           |           |        |                |          |          |

| Cost/foot | R/K  | AWG |
|-----------|------|-----|
| 1         | 5.06 | 14  |
| 1.29      | 3.18 | 12  |
| 1.62      | 2    | 10  |
| 4.47      | 1.26 | 8   |
| 5.78      | 0.81 | 6   |
| 7.62      | 0.51 | 4   |
|           |      |     |

# Hard Wired Communications



Fiber Along Main Feed Line:

OCC Fiber – Arctic Fox Used successfully at the south pole. Flexible to -70C 6 Fibers - \$1.05/ft +/- 5% with 3280 ft minimum

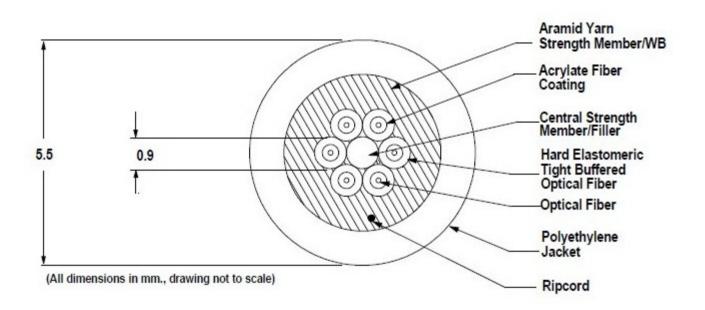
Length: 20580 ft Cost: \$21609.00



Westermo Lynx 1400 Series Switch Rated to -40C Used for redundant ring feature – reduces required fiber count

# «« PROPRIETARY INFORMATION OF OPTICAL CABLE CORPORATION »» DETAIL DRAWING 6-CHANNEL TIGHT BUFFERED DISTRIBUTION FIBER OPTIC CABLE OPTICAL CABLE CORPORATION P/N:

#### D-006ASLS5KAAF \* ARCTIC FOX PLUSTM



# **Hard Wired Communications**



4 Conductor 20 AWG cable run from feed line run from fiber connected station to non fiber connected stations

Westermo DDW-220

Daisychain-able Ethernet Extender

Good to -40C

# **Scaling To Larger Arrays:**

**PLATO** – Plateau Observatory



#### What is Plato?

Stand alone 1 KW diesel generator module

One year service interval ( dome A – running for 580 days unattended )

Developed by the University of New South Wales.

UNSW has over a decade worth of remote power system experience in Antarctica (Plato – AASTINO - AASTO )



Scaling power production up with the UNSW system can be done by adding a larger fuel tank. Scaling up a few more watts with a wind/solar hybrid system has the potential to require a new tower/generator.

#### Costs:

Estimated costs for a ~300 watt version of PLATO is \$88K with an estimated fuel consumption of 150 gallons of diesel for one year

Recurring costs include refueling, oil changes, and replacing diesel engines.

The current design is a diesel / solar hybrid system. It may be possible to further reduce fuel consumption by adding wind turbines to this system to reduce engine hours during the winter.